Thermoelectric (TE) refrigeration in a solid-state active cooling method with high reliability. Bi$_2$Te$_3$-based TE coolers are widely used for cooling and temperature stabilization of microelectronic and optoelectronic devices. SiGeC can be lattice matched to Si and is a promising material for integrated coolers. SiGeC/Si superlattice structures were grown on Si substrates by molecular beam epitaxy. Thermal conductivity was measured by the 3ω method. SiGeC/Si superlattice microcoolers with dimensions as small as 40×40 μm$^2$ were fabricated and characterized. Cooling by as much as 2.8 and 6.9 K was measured at 25 °C and 100 °C, respectively, corresponding to maximum spot cooling power densities on the order of 1000 W/cm$^2$.

Monolithically integrated active cooling is an attractive way for thermal management and temperature stabilization of microelectronic and optoelectronic devices. SiGeC can be lattice matched to Si and is a promising material for integrated coolers. SiGeC/Si superlattice structures were grown on Si substrates by molecular beam epitaxy. Thermal conductivity was measured by the 3ω method. SiGeC/Si superlattice microcoolers with dimensions as small as 40×40 μm$^2$ were fabricated and characterized. Cooling by as much as 2.8 and 6.9 K was measured at 25 °C and 100 °C, respectively, corresponding to maximum spot cooling power densities on the order of 1000 W/cm$^2$.

In this letter, we report the experimental results on SiGeC/Si superlattice microcoolers. Superlattice structures can improve the cooler performance by reducing the thermal conductivity between the hot and the cold junctions and by selective emission of hot carriers above the barrier layers in the thermionic emission process. Si-based microelectronic devices can be monolithically integrated with these coolers to achieve better performance and reliability.

The SiGeC/Si superlattice sample was grown in a Perkin–Elmer Si molecular beam epitaxy (MBE) system capable of codepositing Si, Ge, and C onto 5 in. Si substrates. Solid Si, Ge, and C were evaporated through the use of e-beam sources controlled by electron impact emission sensors (Si, Ge) and by monitoring atomic mass unit 36 (C$_3$) with a quadrupole mass spectrometer (C). Prior to loading into the MBE system, 125 mm diameter, (001)-oriented Si substrate, doped to <0.005 Ω·cm with As, was stripped using 5% hydrogen fluoride. After rinsing with deionized water, the wafer was loaded in the MBE chamber. In order to remove any remaining oxide and to prepare the sample for epitaxial growth, the substrate was heated to 850 °C and exposed to a 0.1 Å/s Si flux for 30 s.

The structure consisted of a 2 μm thick Si$_{0.89}$Ge$_{0.10}$C$_{0.01}$/Si superlattice (100 periods, each sublayer...
10 nm in thickness) grown at 500 °C, lattice matched to the Si substrate. The superlattice was doped with Sb to approximately $2 \times 10^{19}$ cm$^{-3}$. Finally, the sample was capped with 100 nm Si:Sb, grown at 460 °C and doped to approximately $1 \times 10^{20}$ cm$^{-3}$. A cross sectional transmission electron microscopy image of a grown SiGeC/Si superlattice cooler sample is shown in Fig. 1.

The thermal conductivity is a key parameter for thermoelectric materials. The TE device performance increases with a decrease in thermal conductivity. Thin films and nanostructures have been used to reduce the thermal conductivity via acoustical phonon confinement and interface scattering. The $3\omega$ method was used to measure the cross-plane thermal conductivity of the Si$_{0.89}$Ge$_{0.10}$C$_{0.01}$/Si superlattice. The result is $0.085$ W/cm K, which is over one order lower than that of Si ($1.5$ W/cm K).

The processing of SiGeC/Si microcoolers is compatible with an integrated circuit fabrication process. The schematic diagram of the cooler device structure is shown in Fig. 2. Microcoolers were thermally isolated by dry etching mesa structures down to the $n^+$ Si substrate. Metallization was made on the mesa and the Si substrate for cathode and anode contacts, respectively. The main part of the cooler structure is the 2 μm thick superlattice. Its low electrical resistance requires low contact resistance for optimum device performance. Ti/Al metallization was used for ohmic contact. This was followed by annealing at 450 °C for 5 s. Specific contact resistivity of $1.5 \times 10^{-7}$ Ω cm$^2$ was measured by transfer length method.

SiGeC/Si superlattice microcoolers with various mesa sizes ranging from 40×40 to 100×100 μm$^2$ were fabricated on one wafer. They were tested on a temperature-controlled heat sink, which was set at a constant temperature during device testing. Device cooling was measured with micro thermocouples on top of the device and was relative to the values at zero current. Figure 3 displays the measured cooling on top of the devices as a function of current with the heat sink at 25 °C. 2.8 K cooling was obtained for the 40×40 μm$^2$ devices. The test results show that the maximum cooling temperature increases as the device size decreases. This cannot be explained with ideal thermoelectric or thermionic models, and is due to the three-dimensional nature of current and heat spreading in the substrate. The Si substrate of the cooler devices is 500 μm thick and its thermal resistance for the micro devices is about inversely proportional to the square root of the device area. On the other hand, the thermal resistance of the SiGeC/Si superlattice layer is inversely proportional to the device area. This different size dependence makes the effect of the nonideal heat sink smaller for smaller size devices.

For comparison, Si microcoolers were fabricated on $n^+$ Si substrates with similar device structure and processing. The results of the 40×40 μm$^2$ Si devices are shown in Fig. 4 along with those of the SiGeC/Si superlattice coolers of the same size. Over three-fold improvement in maximum cooling is observed for SiGeC/Si superlattice coolers over Si ones.

SiGe is a good TE material for high temperature applications. The SiGeC/Si microcoolers also show better performance at higher temperatures. Figure 5 shows the measured cooling for 50×50 μm$^2$ SiGeC/Si microcoolers at various heat sink temperatures. The maximum cooling increases from 2.5 K at 25 °C to 6.9 K at 100 °C.

The maximum cooling power density is given by

$$Q = \kappa (\Delta T_{\text{max}} - \Delta T)/d,$$

where $\kappa$ and $d$ are the thermal conductivity and the thickness.
of the superlattice, while $\Delta T_{\text{max}}$ and $\Delta T$ are the maximum and actual cooling temperature across the superlattice. At zero $\Delta T$, the coolers have the largest cooling power. Since the majority of the cooling happens over the 2 $\mu$m SiGeC/Si superlattice layer, several degrees of cooling corresponds to maximum cooling power densities on the order of 1000 W/cm$^2$ at zero temperature difference.

The maximum cooling temperature of the SiGeC/Si superlattice microcoolers is limited by the contact resistance, Joule heating and heat conduction from the metal wire connected to the cold junction of the cooler, and the low ZT of the Si substrate. These can be solved by increasing the superlattice thickness, making $n$-type and $p$-type cooler arrays and substrate removal, respectively. Fundamentally, the cooler performance is determined by the TE ZT of the cooler materials. A superlattice gives more freedom in material engineering both electrically and thermally, and enables one to enhance the thermoelectric cooling by thermionic emission, quantum confinement, carrier pocket engineering, and phonon engineering. The structure and doping of the SiGeC/Si superlattice studied here have not been optimized yet. With optimized material and device design and packaging, cooling up to tens of degrees is possible. Furthermore, SiGeC/Si superlattices can be lattice matched to Si, and SiGeC/Si microcoolers can be monolithically integrated with Si-based devices to achieve compact and efficient localized cooling.

In summary, a lattice matched SiGeC/Si superlattice was grown on Si by MBE and SiGeC/Si superlattice microcoolers were demonstrated. Cooling by as much as 2.8 and 6.9 K was measured at heat sink temperatures of 25$^\circ$C and 100$^\circ$C, respectively, corresponding to maximum cooling power densities on the order of 1000 W/cm$^2$.

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